



# Neutronic Simulation of Curved Fuel Plate with Flat Plate Geometry

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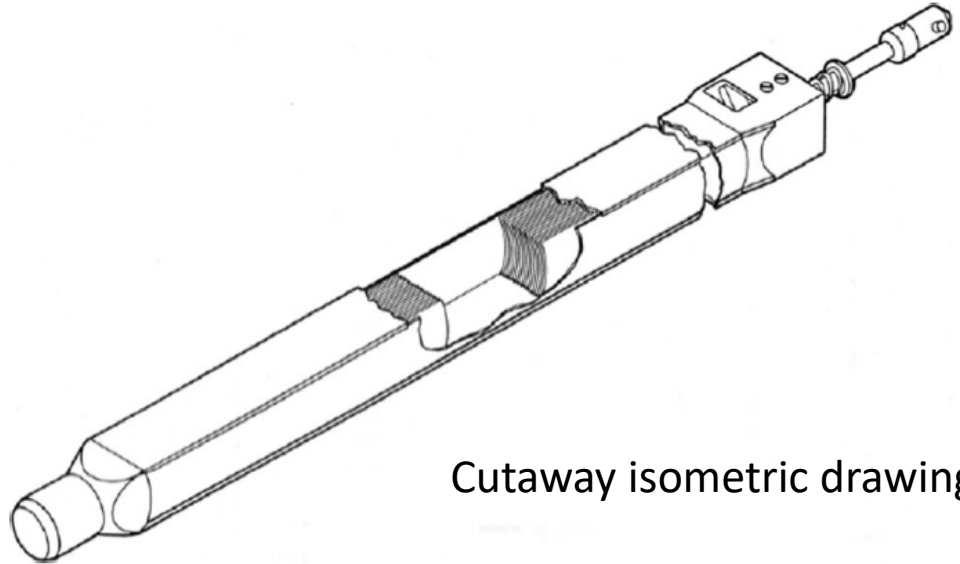


# Outline of Presentation

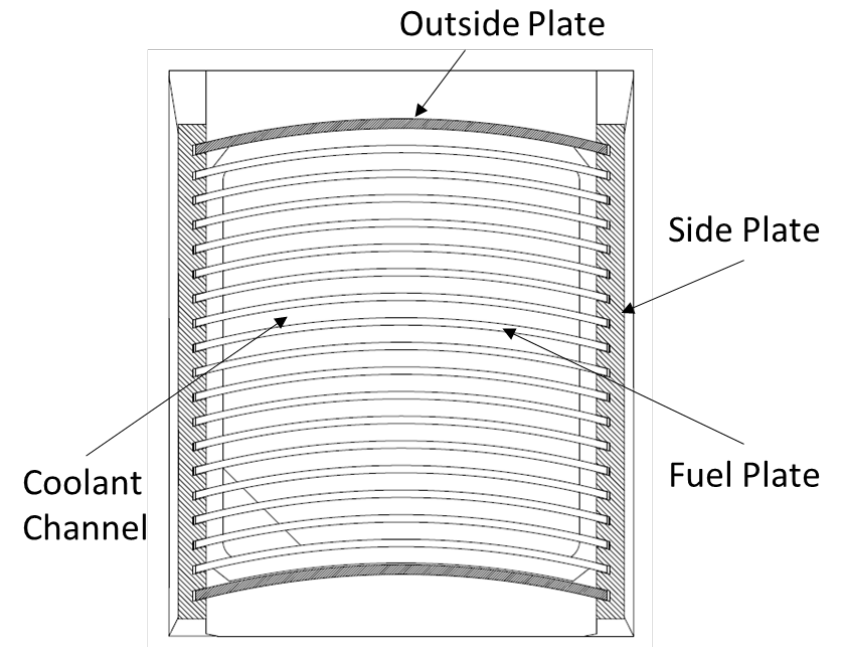
- Objective – demonstrate equivalence of curved-plate and flat-plate model
- NBSR fuel element – geometry and neutronic model
- Single element curved fuel plate model
- Equivalent flat fuel plate model
- Comparison of results –  $K_{eff}$  at start up and through a fuel cycle
- Impact of increased fuel plate curvature
- Summary and conclusion

# The NBSR (1)

- ❖ The NBSR
  - Is a heavy-water ( $D_2O$ )-moderated-and-cooled tank-type reactor operating at the NIST
  - Uses 30 MTR plate-type fuel elements in the core
  - Operates at a nominal thermal power level of 20 MW
  - Has elements with an overall length of 1.75 m. Upper and lower fuel sections are separated by a 17.78 cm gap to maximize the thermal neutron flux
  - Has 17 fuel plates in each fuel section

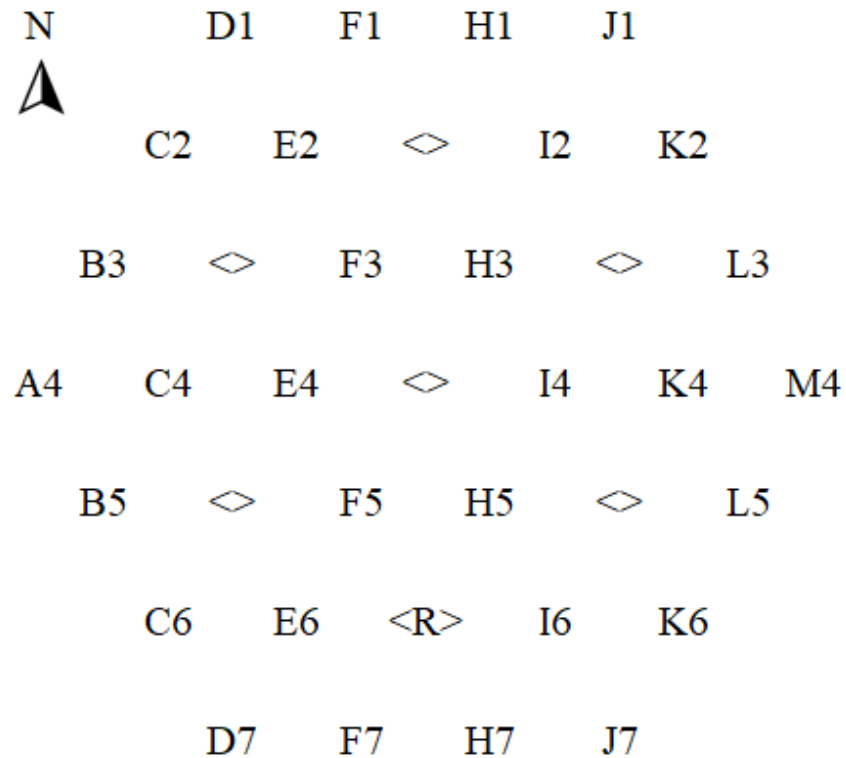


Cutaway isometric drawing

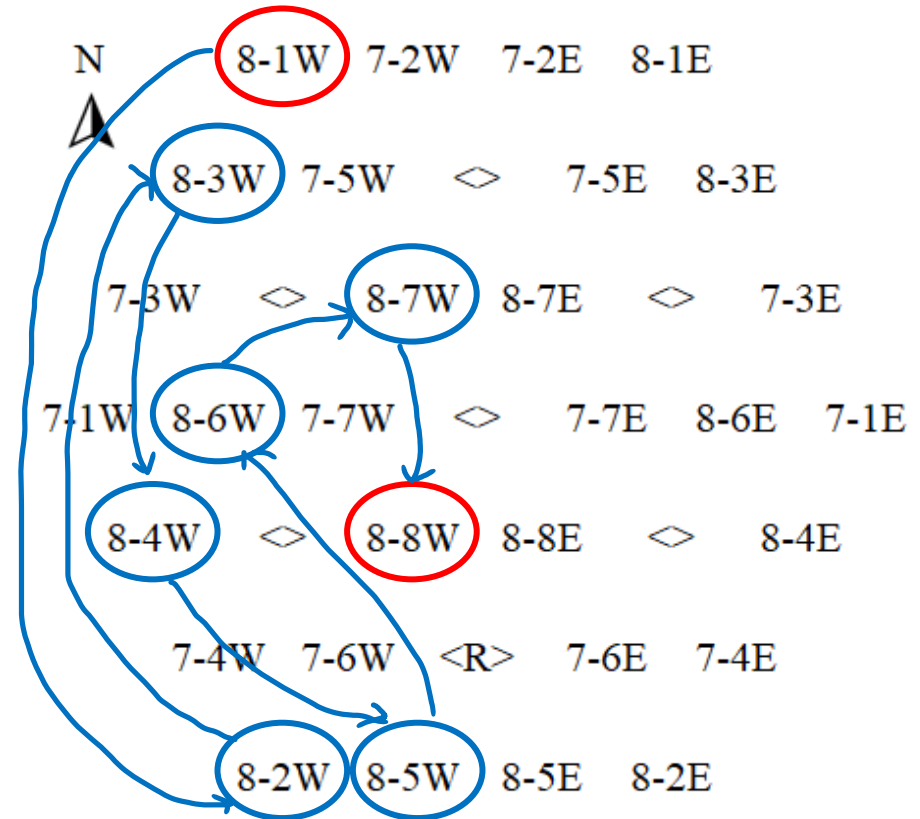


Cross-sectional view

## The NBSR (2)



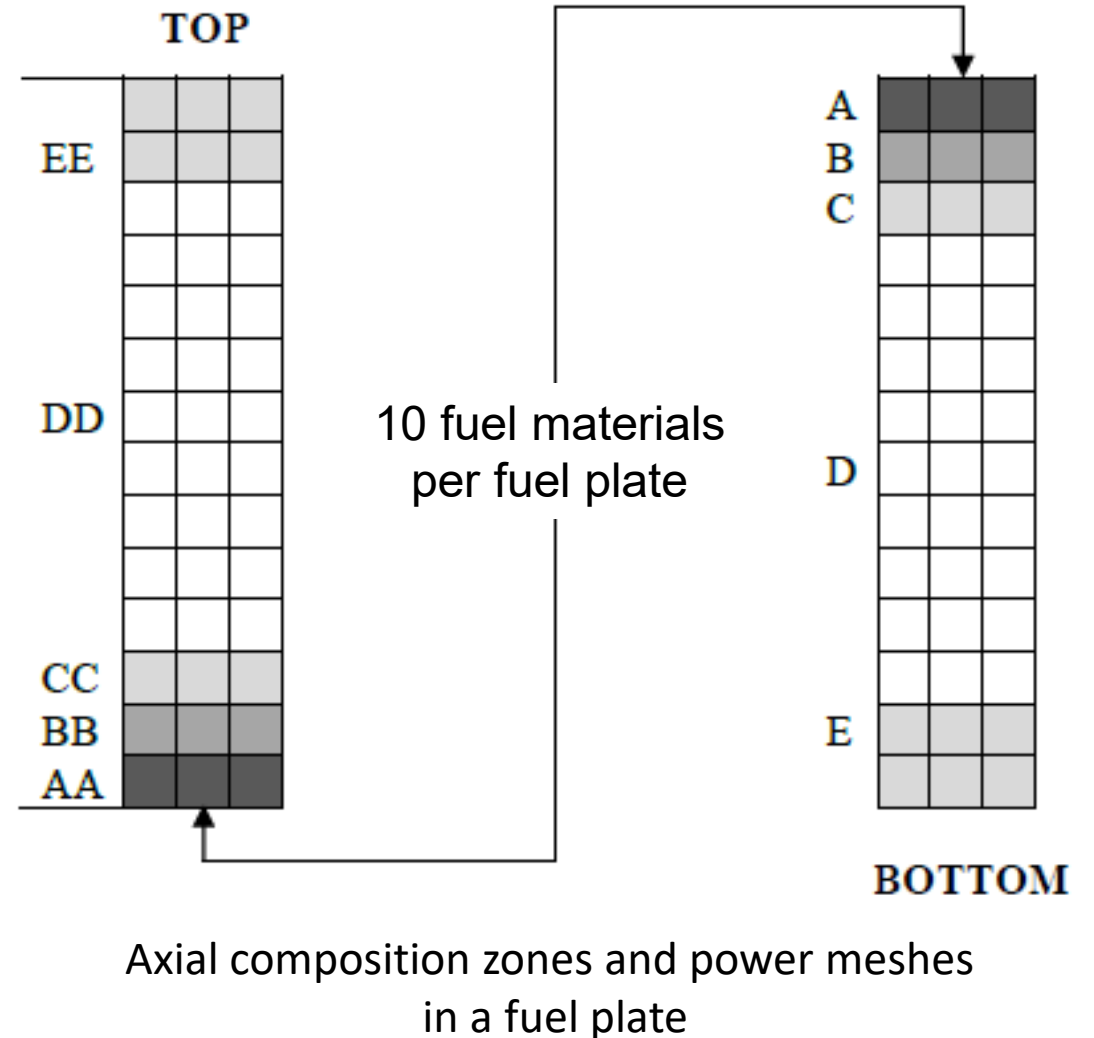
- ❖ Positions of the 30 fuel elements
- <R> represents the regulating rod
- <> represents the in-core irradiation thimbles (6 in total).



- ❖ Fuel shuffling scheme
- The first number (7 or 8) -> total number of cycles
- The second number (1 to 8)-> current cycle
- W (west) and E (east)

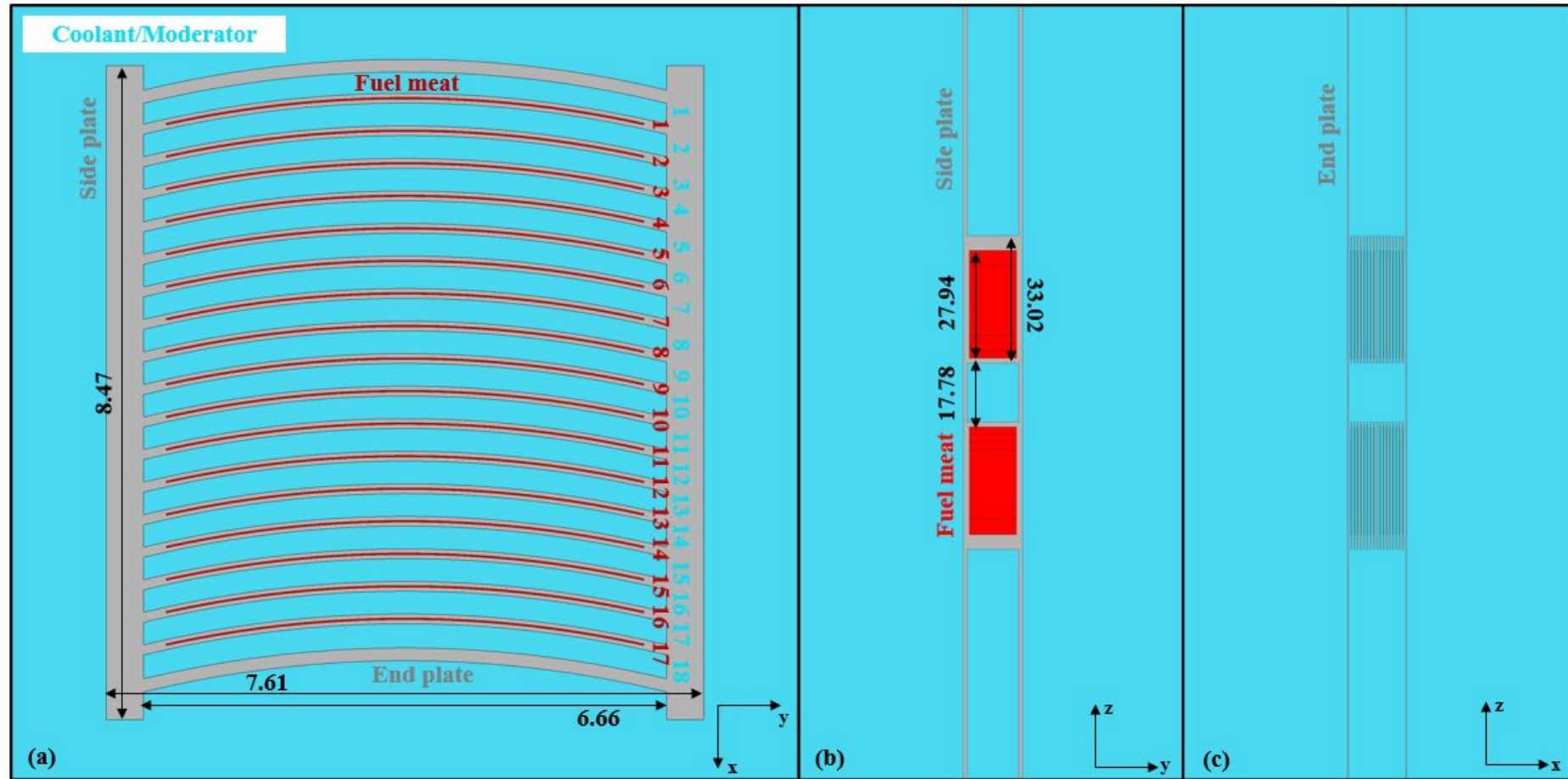
# The NBSR Neutronics Model Fuel Compositions

- ❖ Axial and transverse zones
  - Each fuel plate is broken into 14 axial meshes
  - And 3 transverse meshes for calculating power distribution
  - ~2x2 cm mesh
- ❖ Plate-by-plate material zones
  - 180° symmetry
  - Plates 1 and 17 -> same compositions
  - Plates 2 and 16 -> same compositions
  - Plates 3 - 15 -> same compositions
  - 10 fuel materials per fuel plate
  - In total:  $10 \times 3 \times 30 = 900$  fuel materials



# The Single-element Curved-fuel-plate Model (1)

- ❖ Model constructed according to the NIST LEU NBSR design drawings
- ❖ Two neutronics codes were used, Serpent 2 and MCNP 6.2

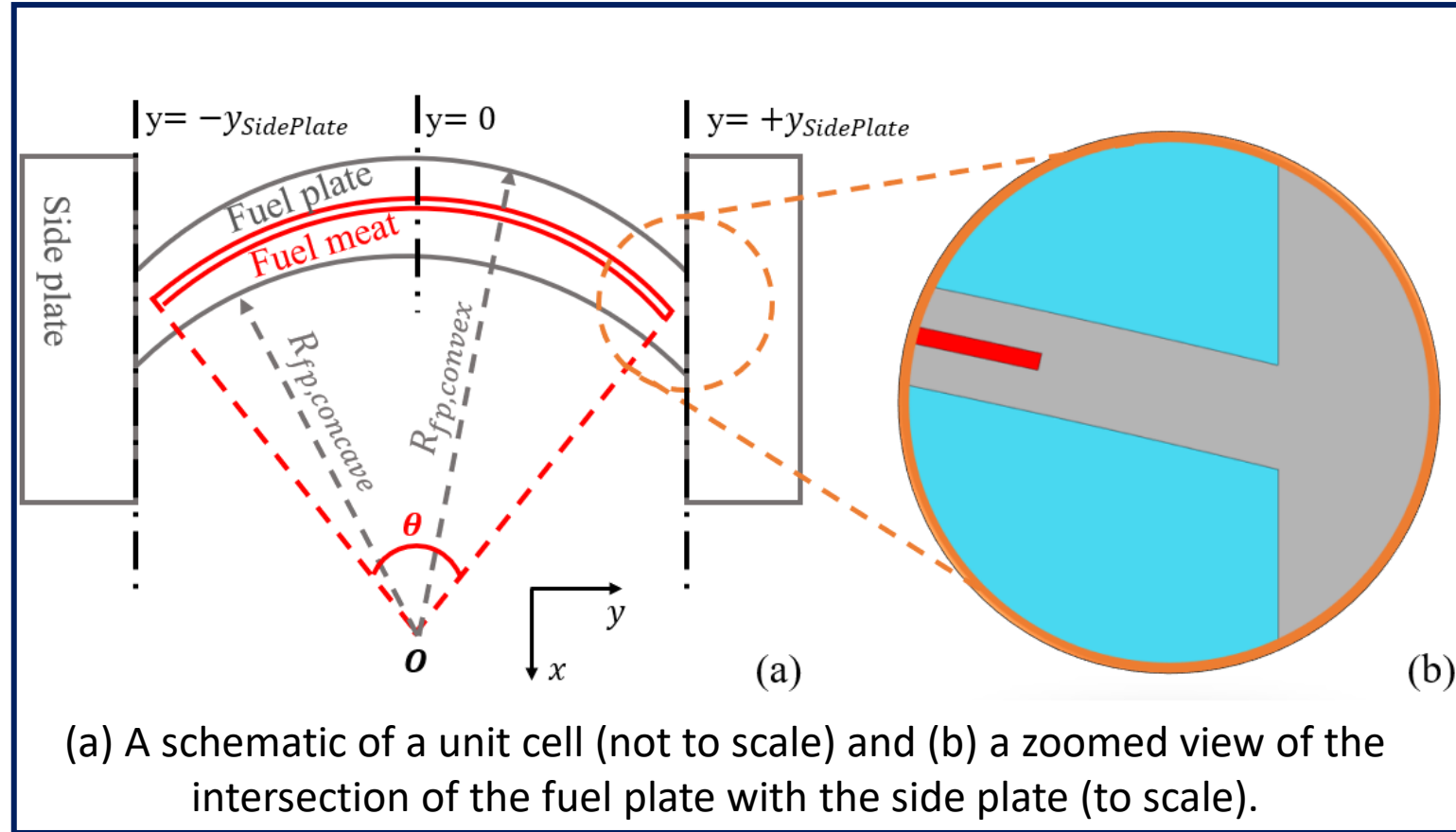


The (a) x-y, (b) y-z, and (c) x-z cross-sectional views of the Serpent 2 model of the reference NBSR fuel element (dimensions are shown in cm)

## The Single-element Curved-fuel-plate Model (2)

- ❖ Calculations of the fuel meat and fuel plate cross-sectional areas
- The fuel meat's degree of curvature ( $\theta$ )  $25^\circ$  from the specified fuel meat x-y cross-sectional area ( $A_{fm}$ ) by solving
 
$$\theta/2 \times (R_{fm,convex}^2 - R_{fm,concave}^2) = A_{fm}$$
- The fuel plate x-y cross-sectional area ( $A_{fp}$ ) was calculated by analytically integrating

$$\int_{-y_{SidePlate}}^{+y_{SidePlate}} \left( \sqrt{R_{fp,convex}^2 - y^2} - \sqrt{R_{fp,concave}^2 - y^2} \right) dy = A_{fp}$$

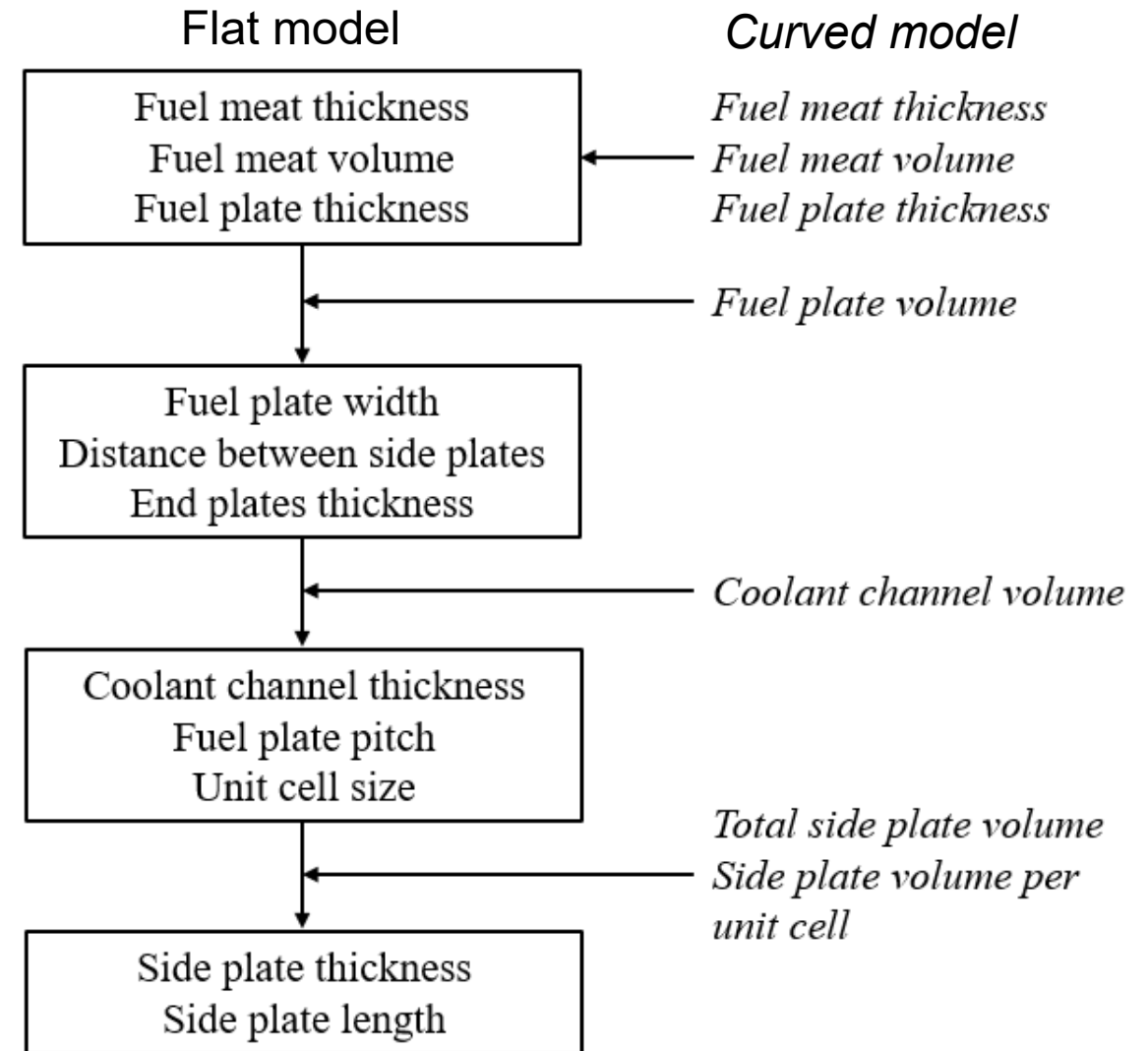


# The Single-element Equivalent Flat-fuel-plate Model

❖ To construct the NBSR single-element equivalent flat-fuel-plate model from the curved-fuel-plate model, the following parameters were explicitly conserved

- Fuel meat thickness
- Fuel meat volume per fuel plate
- Fuel plate thickness
- Fuel plate volume per fuel plate
- Coolant channel volume
- End plate volume
- Side plate volume per unit cell
- Side plate volume per fuel element

❖ The geometry modifications were made on the x-y plane only, while all the z locations remained unchanged



The process of developing the equivalent flat-fuel-plate model



# Equivalence Between the NBSR Single-element Curved-fuel-plate and Equivalent Flat-fuel-plate Models (1)

- ❖ MCNP model for verification
  - Version MCNP6.2
  - Converted surface-by-surface and cell-by-cell from the Serpent 2 model
  - ~500 lines in the flat-plate model
  - ~1000 lines in the curved-plate model
  
- ❖ Agreement within statistical uncertainties (20 pcm), which demonstrates the equivalence between the two models at the equilibrium state.

$k_{\text{eff}}$  of the SU equilibrium **curved-fuel-plate** and **equivalent flat-fuel-plate** models

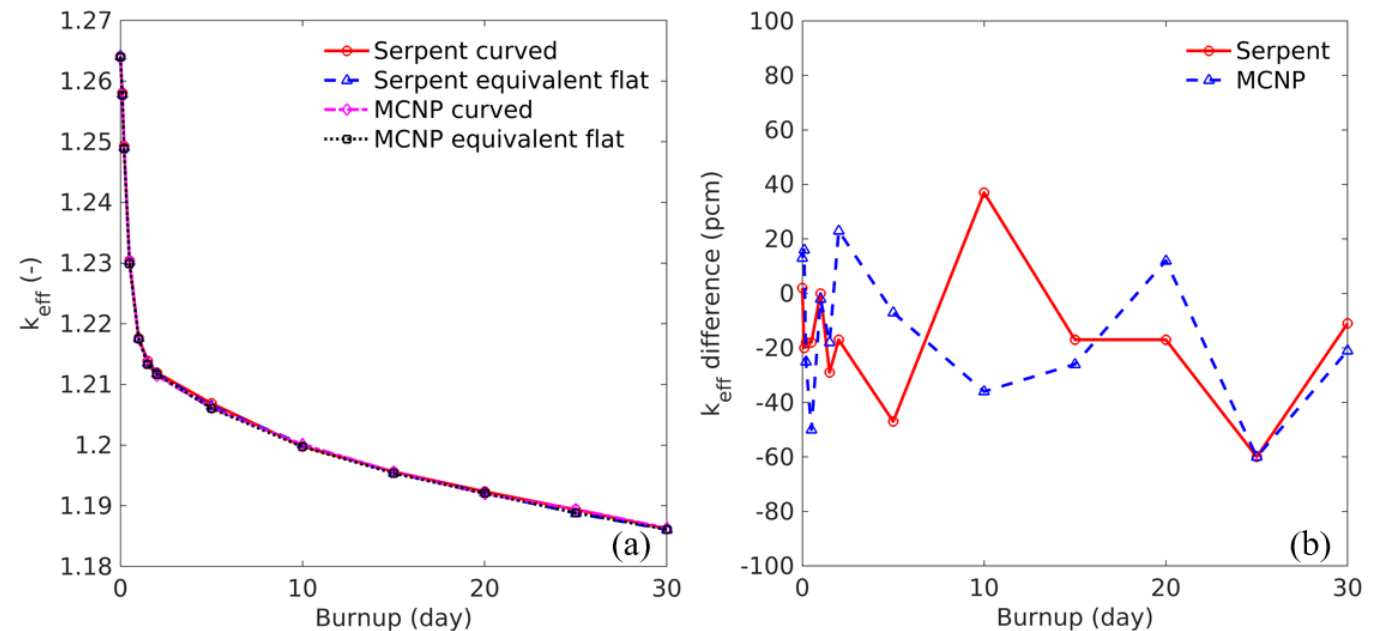
Model	$k_{\text{eff}}$	$k_{\text{eff}}$ uncertainty	$\Delta k_{\text{eff}}$
Serpent curved	1.22473	0.00019	<b>0.00020</b>
Serpent equivalent flat	1.22453	0.00019	
MCNP curved	1.22465	0.00019	<b>0.00015</b>
MCNP equivalent flat	1.22450	0.00018	

# Equivalence Between the NBSR Single-element Curved-fuel-plate and Equivalent Flat-fuel-plate Models (2)

- ❖  $k_{\text{eff}}$  investigated through a postulated 30-day cycle
  - With a whole-element fission power of 0.6667 MW (20 MW / 30 elements)
  - With finer steps at the BOL
- ❖ The absolute differences in Serpent and MCNP  $k_{\text{eff}}$ 
  - Oscillated around zero
  - Maximum  $\sim 60$  pcm
  - Arrived at around 20 pcm at the EOC
- ❖ Demonstrates the equivalence between the two models through a fuel cycle

Fresh fuel isotopic composition (LEU)

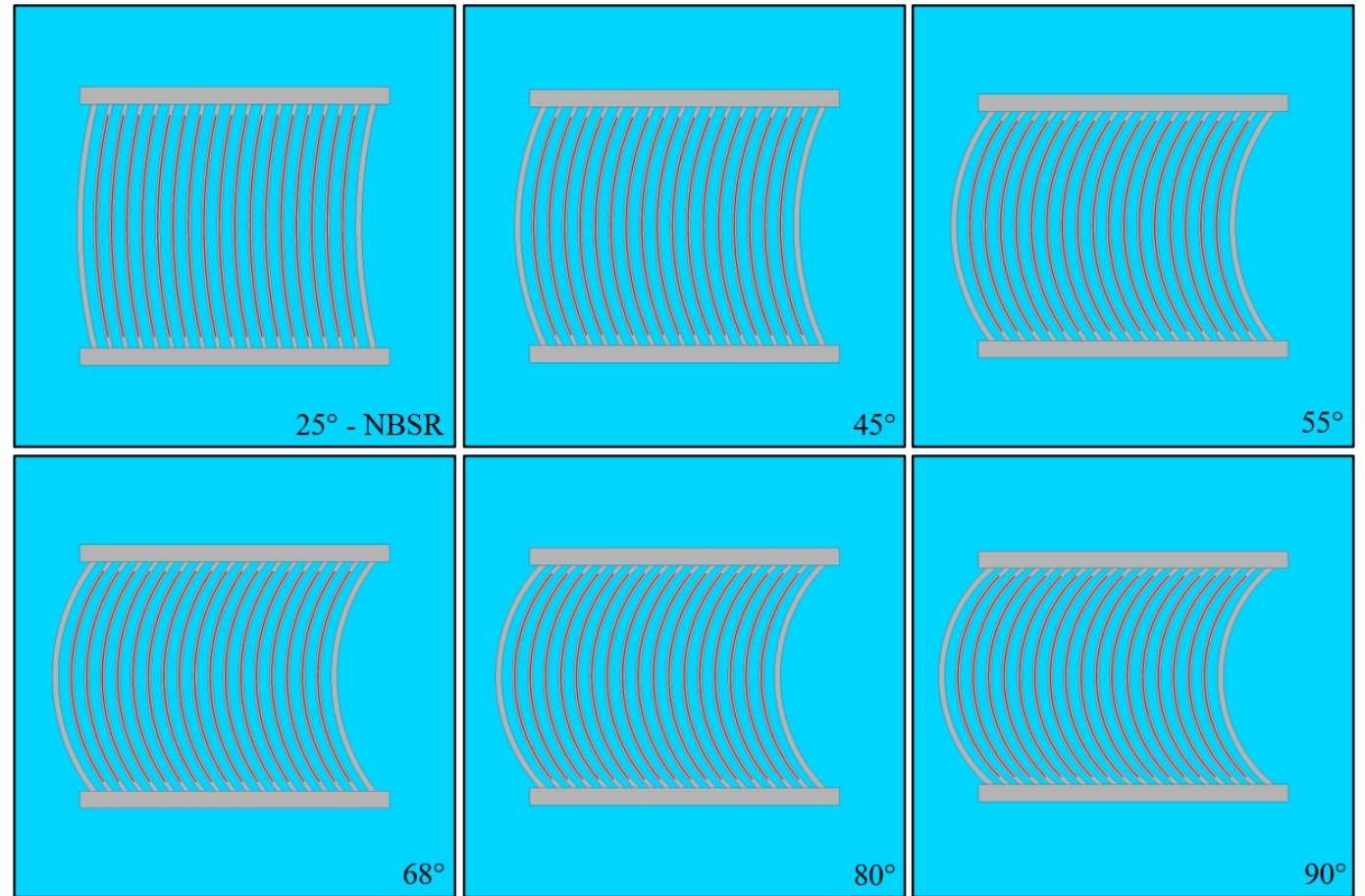
	$^{235}\text{U}$	$^{238}\text{U}$	Mo	Total
Mass in the element (g)	383	1556	215	2154
Mass density (g/cm <sup>3</sup> )	3.06	12.42	1.72	17.19
Weight fraction (%)	17.78	72.24	9.98	100



(a)  $k_{\text{eff}}$  and (b) difference in  $k_{\text{eff}}$  of the NBSR single-element models through a postulated 30-day fuel cycle (equivalent flat-fuel-plate model - curved-fuel-plate model)

# Impact of the Fuel Plate Curvature on the Equivalence Between the Curved-fuel-plate and Equivalent Flat-fuel-plate Models (1)

- ❖ To discuss the validity of approaching the equivalence when larger plate curvatures are considered for
  - Current RTR power upgrades
  - Future RTR designs
- ❖ Increase in plate curvature realized by shortening the distance between the side plates
  - Coolant channel volumes decreased
  - Volumes of the other components of the fuel elements remained unchanged

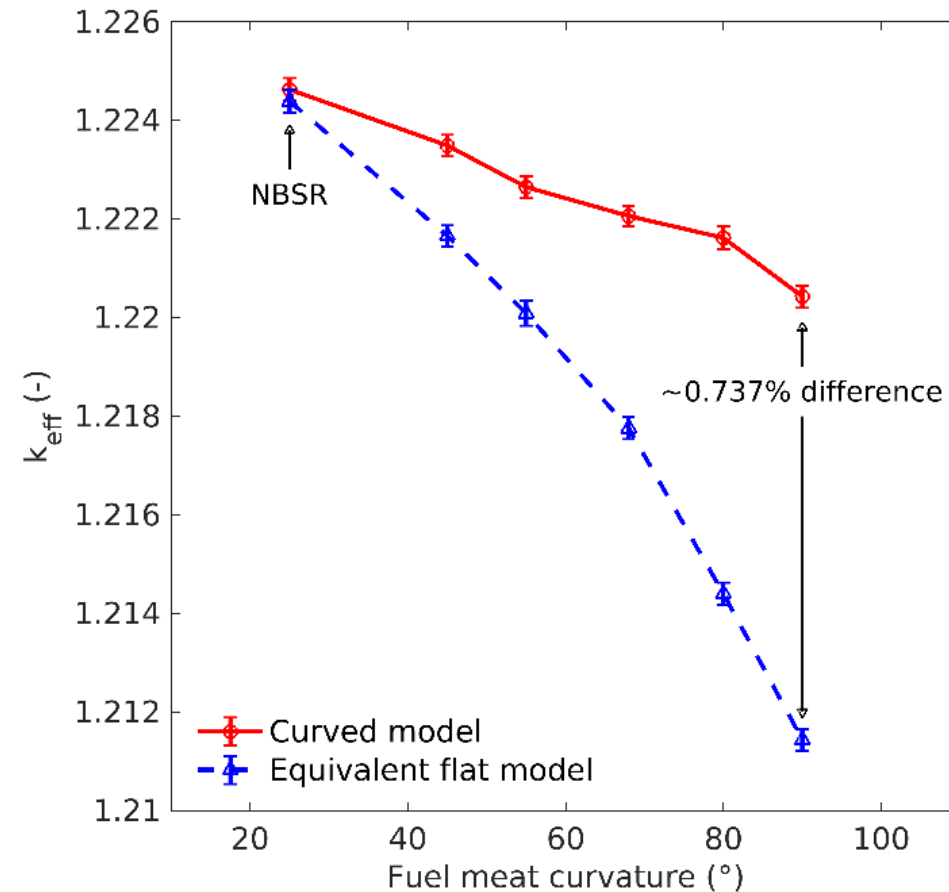


The x-y cross-sectional views of the Serpent 2 models of the six fuel elements with different curvatures

# Impact of the Fuel Plate Curvature on the Equivalence Between the Curved-fuel-plate and Equivalent Flat-fuel-plate Models (2)

## ❖ Findings

- $k_{eff}$  of the 25° fuel element design was approximated within 20 pcm
- The equivalent flat-fuel-plate model underpredicted the  $k_{eff}$  when the fuel meat curvature became larger.
- The underprediction reached 0.737% for the 90° cases
- This would be 737 pcm if the 90° curved-fuel-plate model were critical



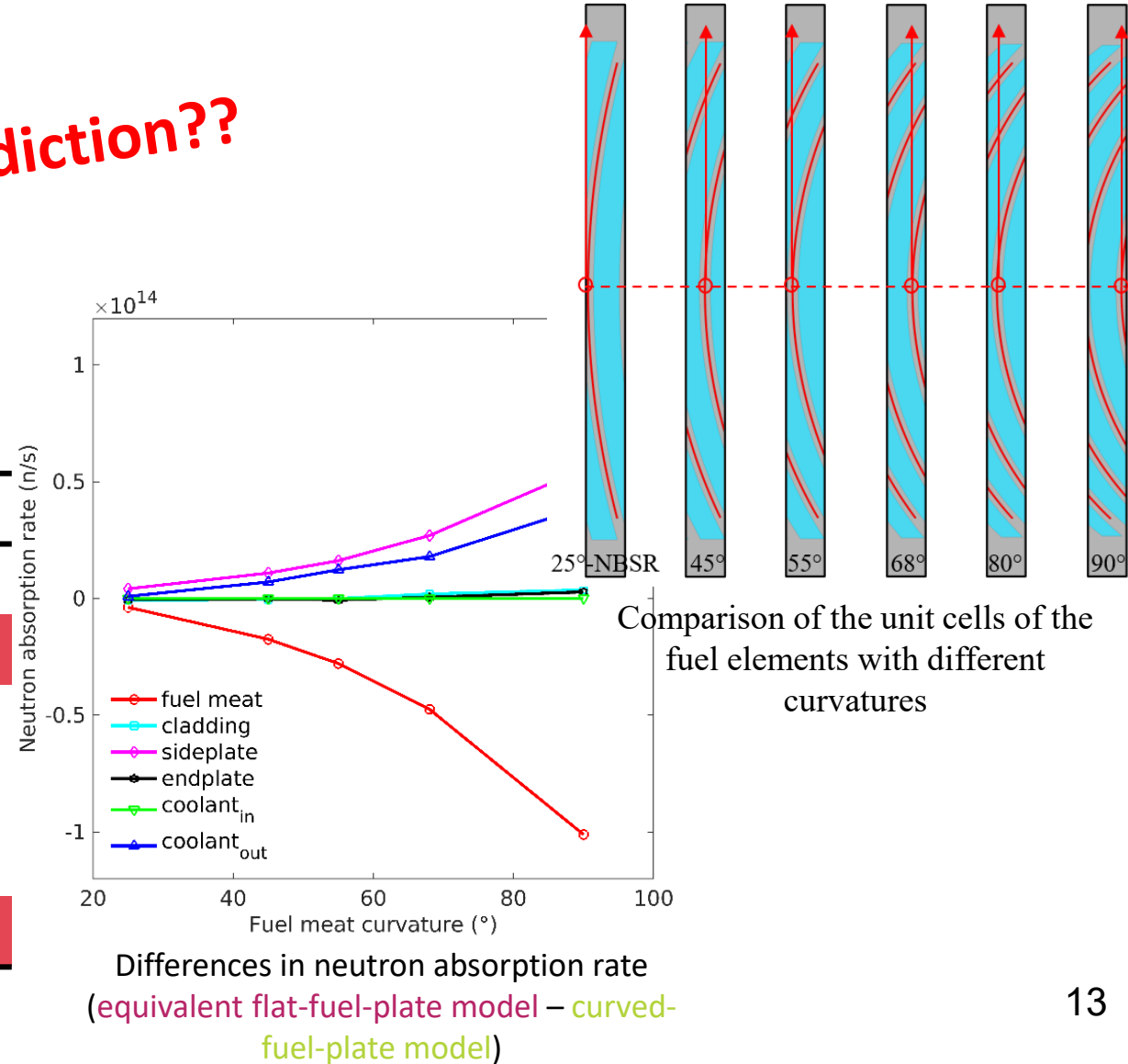
Comparison of the  $k_{eff}$  of the curved-fuel-plate models with those of the equivalent flat-fuel-plate models

# Impact of the Fuel Plate Curvature on the Equivalence Between the Curved-fuel-plate and Equivalent Flat-fuel-plate Models (3)

What caused the underprediction??

The relative differences of the six-factor-formula factors for different curvatures (equivalent flat-fuel-plate model – curved-fuel-plate model)

	25°	45°	55°	68°	80°	90°
$\eta$	5.03E-05	9.57E-05	1.86E-04	7.05E-05	-4.18E-04	-1.71E-04
$f$	-2.05E-04	-1.11E-03	-1.20E-03	-2.09E-03	-2.97E-03	-3.99E-03
$p$	-1.68E-05	-2.45E-04	-6.31E-05	-6.83E-05	-1.33E-04	-2.04E-04
$\epsilon$	5.79E-05	2.61E-04	2.51E-04	2.90E-04	4.63E-04	6.18E-04
$L_F$	6.00E-06	0.00E+00	-4.00E-06	-1.00E-06	-3.00E-06	-5.00E-06
$L_T$	-9.45E-05	-4.87E-04	-1.25E-03	-1.72E-03	-2.85E-03	-3.62E-03



# Summary

- ❖ The equivalence between an NBSR LEU single-element **equivalent flat-fuel-plate model** and an NBSR LEU single-element **curved-fuel-plate model** was demonstrated with Serpent 2 and MCNP6.2.
- ❖ Study was extended to cover larger plate curvatures. Findings included
  - $k_{\text{eff}}$  of the 25° fuel element design was approximated within 20 pcm
  - The **equivalent flat-fuel-plate model** underpredicted the  $k_{\text{eff}}$  when the fuel meat curvature became larger.
  - The underprediction reached 0.737% for the 90° caseswhich emphasized the importance of understanding the uncertainties caused by modeling **curved fuel plates** with equivalent **flat fuel plates** for neutronic calculations.
- ❖ Plan to build an NBSR LEU whole-core **curved-fuel-plate model** for future LEU NBSR analysis to reduce the uncertainties in  $k_{\text{eff}}$  calculations.